

"Bicycle wheel hub"

This invention relates to a method for fabricating the hub of a bicycle wheel, an apparatus for implementing the method and the bicycle wheel hub
5 obtained by means of the said method.

The Applicant has recently conducted various studies and tests to make bicycle components, particularly bicycle wheel hubs, especially for spoke wheel competition bicycles, using structural fibre
10 based material, typically carbon fibre based material. The advantage offered by this type of material is that of being lighter in weight with respect to the metallic materials used in the past given equal structural characteristics. Making a hub out of a single part of
15 carbon fibre based material was difficult, at least utilising the technologies available at that time, due to the typical conformation of the bicycle wheel hub of the type described above. The hubs used in modern bicycle wheels present a complex cylindrical shape,
20 with a central constant diameter section and two bell-shaped end sections with a wider diameter or other, even more complex, shapes. Additionally, it is desirable for the hub thickness to progressively increase from the central section towards the hub ends,
25 so to ensure the necessary resistance characteristics in all areas of the hub, particularly on the ends, where the wheel spokes are anchored, while ensuring minimal weight at the same time.

The need of making a tubular body with the complex
30 shapes described above has made it impossible to make the hub from a single part of structural fibre material, such as carbon fibre material.

The object of this invention is to overcome this technical problem.

35 In view of achieving this object, the invention

provides a method for fabricating a bicycle wheel hub, characterised in that it comprises the following steps:

- providing an expandable core,
- applying a number of layers of structural
5 fibre fabric incorporated in a plastic material matrix around the core to form a layered tubular body of predetermined shape and thickness around the core,
- arranging the core with the layered tubular body formed thereon in the cavity of a mould,
- 10 - increasing the temperature of the mould to a value sufficient to cause reticulation of the plastic material matrix,
- expanding the core for applying a pressure on the tubular body inside the mould, and
- 15 - removing the tubular body from the mould and from the core, so as to obtain a bicycle hub formed of a single piece of structural fibre material.

In a first embodiment, the expandable core is made of a synthetic material presenting a thermal dilatation
20 coefficient exceeding 5×10^{-15} mm/°C and a maximum continuous heat resistance equal to at least 80°C, the expansion of the core being obtained through the dilation of the material forming the core when the temperature of the mould is increased.

25 Preferably, in this embodiment, the material forming the core has a thermal dilation coefficient exceeding 9×10^{-5} mm/°C and a maximum continuous thermal resistance temperature exceeding 100°C.

Again preferably, the material forming the core
30 can be either PTFE (polytetrafluoroethene), or FEP (fluorinated ethene propene), or PCTFE (polychlorotrifluoroethene), or PVDF (polyfluorodivinyldene), or PE-HD (high density polyethylene).

35 The use of PTFE is widely preferred, due to the

anti-adherence properties of this material, which are useful for detaching the core from the structural fibre moulded body, as well as its high continuous thermal resistance (260°C), for its good thermal conductivity (0.25 W/m°C) and for its good thermal capacity (specific heat), equal to 1.045 kJ/kg°C.

The method, which main phases are outlined above, can be used in general to make hubs of all shapes, also different from that described above. A highly preferred characteristic of this method is in the arrangement of the aforesaid core made of high thermal dilation synthetic material, preferably PTFE. This material presents the characteristic of being subject to high thermal dilation at relatively low temperatures, in the order of temperatures at which the plastic material in which the structural fibre fabric is incorporated reticulates.

In a second embodiment of the method of the invention, the expandable core includes a body of metal material covered with a deformable sheath made of an elastomeric material, the expansion of the core being obtained through the dilation of the material forming the sheath when the temperature of the mould is increased.

Preferably, in this embodiment, the elastomeric material forming the aforesaid sheath has a thermal dilation coefficient exceeding 15×10^{-5} mm/°C and a maximum continuous heat resistance temperature exceeding 100°C. Still preferably, this material is a synthetic rubber of the type marketed under the trademark AIRCAST 3700 by Airtech International Inc., Huntington Beach, California, USA.

According to a further preferred feature of the second embodiment, the sheath is pre-formed according to the configuration of the core and is dimensioned in

order to be applied on the core by slightly stretching it, so that the sheath adheres to the core due to its elasticity.

In a third embodiment of the method of the invention, the expandable core includes a body of metal material without any deformable sheath. In this embodiment the metallic core is divided in sectors, which can be expanded by means of mechanical means or, if provided by elastomeric junctions, by means of a gas injected inside the metallic core.

Structural fibre fabrics incorporated in a plastic material matrix are known and have been used for some time. They are made with yarn obtained from structural fibres, such as carbon fibres, for example. These fabrics are then subjected to a calendering process to associate them to a plastic material matrix, typically a thermosetting plastic material.

In the method of the invention, the structural fibres are selected among carbon fibres, glass fibres, Kevlar fibres, or any combinations thereof.

According to another important feature of the invention, the layers of fabric on the core comprise one or more fabric strips wrapped around at least one axially limited portion of the core, to confer thickness to the tubular body, as well as a plurality of fabric plies extending along the core axis, to confer resistance in the axial direction to the tubular body.

Further features of the method of the invention are indicated in the appended claims 23-34.

This invention also relates to an apparatus as set forth in claims 41-44.

Finally, this invention also relates to a bicycle wheel hub, characterised in that it has a tubular body made of a plurality of layers of structural fibre

fabric incorporated in a plastic material matrix, said layers including one or more fabric strips wrapped around at least one axially limited portion of the hub body as well as a plurality of fabric plies extending
5 along the hub axis.

This invention will be better explained by the following detailed descriptions with reference to the accompanying figures as non-limiting examples, whereas:

- figure 1 generally indicates a perspective
10 view of the core belonging to the apparatus used in the method according to a first embodiment of this invention,

- figure 2 illustrates a perspective view of the two elements forming the core in figure 1 in a reciprocally distanced condition,
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- figures from 3 to 15 are perspective views illustrating the various phases of applying the layers of the carbon fibre fabrics on the core shown in figure 1,

20 - figure 16 is a perspective view illustrating the core in figure 1 completely coated with layers of carbon fibre fabrics,

- figure 17 is a partial cross-section view of the assembly illustrated in figure 16, with two
25 elements forming the core and the pre-formed tubular layered body over them,

- figure 18 is a cross-sectional view of the mould usable in the method according to the first embodiment,

30 - figures 19,20 are variant of figures 17,18 corresponding to a second embodiment of the invention,

- figure 21 is a perspective view of the sheath of elastomeric material which is used in the method
35 according to the second embodiment, and

- figure 22 shows wheel hubs with different shapes.

With reference to figure 1, numeral 1 generically indicates a generally cylindrical core, consisting of two separate elements 3, 4. In the example shown, each of the two elements 3, 4 is made of a single piece of PTFE. In the closed condition illustrated in figure 1, the two elements 3, 4, form a substantially cylindrical core, with a central section 2 presenting a constant diameter and two bell-shaped end sections 5, 6 with an enlarged diameter, ending with two ring flanges 7, 8.

With reference to figures from 3 to 16, the core 1 is externally coated with layers of structural fibre based fabric (typically carbon based fabric) incorporated in a thermosetting plastic material matrix. The various phases of the layering process are illustrated in the figures from 3 to 15.

With reference to figure 3, in a first phase, a strip 50 of carbon fibre fabric is wrapped around on bell-shaped end 5 of the core 1 (e.g. five complete turns around the core). After this, the same operation is carried out on the strip of fabric 51 over the end 6 of the core 1. Figure 4 illustrates the core 1 with two windings 50, 51 obtained at the end of the aforesaid phase.

The strips 50 and 51 present triangular cuttings 50' and 51' to allow to such strips to enclose a tubular area with different diameters without leaving empty spaces or forming overlappings.

A first piece, or ply, 52, a second ply 53 (figure 5), a fourth ply 54 and a fifth ply 55 (figure 6) are then applied to the body thus obtained in four subsequent phases. All the plies 52, 53, 54, 55 extend for the entire axial length of the core, while each one only partially covers the core in the circumferential

direction. As can be seen in figures 5, 6, they are applied on four different sides, arranged at an angle of 90° one with respect to the other. Firstly, two plies 52, 53, which are diametrically opposite are applied, after which two other plies 54, 55, which are also diametrically opposite and oriented at 90° with respect to the plies 52, 53 are applied. In this way a couple of plies cover the entire circumference of the tubular body and the junctions of two couples of plies are alternated, in particular spaced apart of 90° . Figure 7 illustrates the structure obtained at the end of the phases illustrated in figures 5, 6. The function of the plies described above is very important, because the plies connect the strips on the end of the core thus providing axial resistance to the layered body.

At the end of the phase described above, two strips 56, 57 (presenting triangular cuttings 56' and 57' - figure 8) are wrapped over the applied layers in subsequent phases, in correspondence to the ends of the core so to obtain the structure shown in figure 9. At this point, two additional strips 58, 59 (presenting triangular cuttings 58' and 59') are additionally wrapped over the end of the core (figure 10), after which two additional plies 60, 61, (presenting triangular cuttings 60' and 61') which are diametrically opposite and which shape is shown in figure 11 are applied. The plies 60, 61 are obviously applied in two subsequent moments, to obtain the structure shown in figure 12, where said plies join the end layers so to additionally increase the axial resistance of the layered body.

The method ends with the application of two additional strips 62, 63, (presenting triangular cuttings 62' and 63') which shape is shown in figure 13, which are wrapped around the ends of the core in

two subsequent moments so to obtain the structure visible in figure 14, after which a last strip 64 is applied, which shape is shown in figure 15, and wrapped around the central part of the core, so to finally
5 obtain the structure shown in figure 16.

The illustrated strips 50, 51, 56, 57, 62, 63 present triangular cuttings 50', 51' 56', 57', 62' 63' on one side, but they could present triangular cuttings on both sides. Said strips can also present, on one or
10 on both sides, cuttings of other shapes, such as circular, oval, squared, rectangular, rectilinear and so on, or any combination thereof, the cuttings being perpendicular or inclined with respect to the edges of the strips. Further, it is also possible to choose the
15 number, the depth, the width and the inclination of the cuttings. The strips 50, 51, 56, 57, 62, 63 could also present, on one or on both sides, extensions of different shapes, such as circular, oval, squared, rectangular, triangular and so on, or any combination
20 thereof, the extensions being perpendicular or inclined with respect to the edges of the strips. Further, it is also possible to choose the number, the depth, the width and the inclination of the extensions. Finally, a combination of cuttings and/or extensions, on one or on
25 both sides of the strips can be chosen in such a way as to obtain substantially any kind of thickness and shape such as, for example, the ones showed in fig. 22.

As described, the strips and the plies are arranged alternately with each other, so as to achieve
30 the best result in terms of thickness and axial resistance

Once the method is ended, a tubular body 9 is formed on the core (figure 16) a central constant section 10, and two bell-shaped ends 11, 12, which
35 diameter is larger. Furthermore, the thickness of the

pre-formed tubular body 9 progressively increases from the central section 10 in the direction of the ends or, as can be seen in figure 17, there is a central part (A) of constant section, end parts (C) with constant
5 section, but larger than the central one and intermediate parts (B) with increasing sections. Finally, the two ring end flanges 7, 8 of the core 1 axially contain the ends of the pre-formed tubular body 9.

10 The assembly consisting of the core 1, comprising the two elements 3, 4 and the pre-formed tubular body 9 wrapped around it, is positioned in the cylindrical cavity 13 of a moulding apparatus 14 (see figure 18). The cylindrical cavity 13 is formed by an upper half
15 mould 15 and a lower half mould 16, presenting a conformation which corresponds to that of the external surface of the hub to be obtained, i.e. substantially corresponding to the external surface of the pre-formed tubular body 9 illustrated in figure 16. The ends of
20 the cavity 13 are closed by two caps 17, 18, which are fastened by means of screws 19 to two end flanges of the two half moulds 15, 16. Each of the two caps 17, 18 incorporates a central cylindrical case 20 in which a respective helical spring 21 is arranged. Each of the
25 two helical springs 21 is axially interposed between a bottom wall 20a of the respective tubular case 20 and the respective end surface of the core 1. The two springs 21 elastically press the two elements 3, 4 of the core 1 against each other so that these elements
30 are kept in contact corresponding to their contact plane 22, which is orthogonal to the axis 23 of the core 1.

After arranging the assembly consisting of the core 1 and the pre-formed tubular body 9 wrapped on the
35 core inside the mould, the mould is taken to a

temperature sufficient to cause the reticulation of the thermosetting plastic material matrix belonging to the tubular body 9, for example to a temperature comprised in the range from 80°C to 200°C. This temperature increase is maintained preferably for a time comprised in the range from 10 minutes to 3 hours, preferably in the range from 30 minutes to 3 hours. In this way, the thermosetting matrix reticulates, while the PTFE forming the two elements 3, 4 of the core 1 dilates. This dilation is mainly impressed radially outwards, since the flanges 7, 8 are pressed against the ends of the pre-formed tubular body 9 by the two springs 21. Consequently, a radial pressure is exerted outwards against the tubular body 9, which is thus pushed against the wall of the cylindrical cavity 13. In this way, a uniform pressure is applied on all the parts of the pre-formed tubular body 9, despite the complex conformation of the body illustrated herein, with bell-shaped ends and a progressively increasing thickness, from the centre to the ends. Naturally, during this phase, the springs 21 allow the two elements 3, 4 of the core to distance themselves slightly following the force exerted by the PTFE core against the ring flanges 7, 8.

At the end of the reticulation phase, a cooling phase follows, then the mould is opened and the assembly comprising the core 1 and the body 9 arranged upon it, is extracted. At this point, the elements 3, 4 forming the core 1 are extracted in opposite directions from the body thus obtained, forming the wheel hub according to this invention. The hub thus obtained presents the particularity of being made of structural fibre material, typically carbon fibre material, and being made of a single part, despite the complex geometrical shape described above. The product can

naturally be subjected to additional machining (e.g. a set of radial holes can be drilled in the two bell-shaped ends for engaging the spokes) which make the part usable as a bicycle wheel hub.

5 Many other kinds of hubs with different shapes, illustrated in fig.22, can be obtained. In particular, symmetrical and asymmetrical hubs with respect to the intermediate plane, hubs with one or two flanges in proximity of one or both ends and hubs with cross-
10 shaped flanges.

With reference to figures 19,20 and 21, which relate to a second embodiment of the method of the invention, the core 1 is formed by two elements 3,4 of metal material, e.g. steel, and is externally covered
15 with a sheath 24 made of a high thermal dilatation elastomeric material. Preferably, the elastomeric material forming the aforesaid sheath has a thermal dilation coefficient exceeding 15×10^{-5} mm/°C and a maximum continuous heat resistance temperature
20 exceeding 100°C.

For example, said material forming the core sheath can be a synthetic rubber of the type marketed under the trademark AIRCAST 3700 by Airtech International Inc., Huntington Beach, California, USA. This material
25 is preferred for its relatively high thermal dilation coefficient (15×10^{-5} mm/°C), as well as its high continuous heat resistance (232°C), for its good thermal conductivity (2.59 W/m°C) and for its good ultimate tensile stress (680%), which is important to
30 facilitate removing the sheath from the internal surface of the finished product after extracting it from the module and after removing the core.

The sheath is pre-formed according to the configuration of the core (figure 4) with a central
35 cylindrical section and two bell-shaped end sections

and is preferably dimensioned so to be applied onto the core by stretching it slightly so that the sheath is adherent to the core by effect of its elastic return.

Apart from the above indicated different structure
5 of the core, the method remains identical to that described above with reference to the first embodiment. The assembly consisting of the core 1, comprising the two elements 3, 4, the sheath 24 and the pre-formed tubular body 9 wrapped around it, is positioned in the
10 cylindrical cavity 13 of a moulding apparatus 14 formed by an upper half mould 15 and a lower half mould 16, presenting a conformation which corresponds to that of the external surface of the hub to be obtained, i.e. substantially corresponding to the external surface of
15 the pre-formed tubular body 9 illustrated in figure 21. The ends of the cavity 13 are closed by two caps 17, 18 which are fastened by means of screws 19 to two end flanges of the two half moulds 15, 16. Each of the two caps 17, 18 incorporates a central cylindrical case 20
20 in which a respective helical spring 21 is arranged. Each of the two helical springs 21 is axially interposed between a bottom wall 20a of the respective tubular case 20 and the respective end surface of the core 1. The two springs 21 elastically press the two
25 elements 3, 4 of the core 1 against each other so that these elements are kept in contact corresponding to their contact plane 22, which is orthogonal to the axis 23 of the core 1.

After arranging the assembly consisting of the
30 core 1 and the pre-formed tubular body wrapped on the core inside the mould, the mould is taken to a temperature sufficient to cause the reticulation of the thermosetting plastic material matrix belonging to the tubular body 9, for example to a temperature comprised
35 in the range from 80°C to 200°C. This temperature

increase is maintained preferably for a time comprised in the range from 10 minutes to 3 hours, preferably in the range from 30 minutes to 3 hours. In this way, the thermosetting matrix reticulates, while the synthetic
5 rubber forming the sheath that covers the two elements 3, 4 of the core 1 dilates. This dilation is mainly impressed radially outwards, since the flanges 7, 8 are pressed against the ends of the pre-formed tubular body 9 by the two springs. Consequently, a radial pressure
10 is exerted outwards against the tubular body 9, which is thus pushed against the wall of the cylindrical cavity 13. In this way, a uniform pressure is applied on all the parts of the pre-formed tubular body 9, despite the complex conformation of the body
15 illustrated herein, with bell-shaped ends and a progressively increasing thickness, from the centre to the ends. Naturally, during this phase, the springs 21 allow the two elements 3, 4 of the core to distance themselves slightly following the force exerted on the
20 sheath 24 against the angular flanges 7, 8.

At the end of the reticulation phase, and after a subsequent cooling phase, the mould is opened and the assembly comprising the core 1 and the body 9 arranged upon it, is extracted. At this point, the elements 3, 4
25 and 10 forming the core are extracted in opposite directions from the body, after which the sheath 24, which initially remains associated to the internal surface of the tubular body, is extracted by elastic deformation. The hub thus obtained presents the
30 particularly of being made of structural fibre material, typically carbon fibre material, and being made of a single part, despite the complex geometrical shape described above. The product can naturally be subjected to additional machining (e.g. a set of radial
35 holes can be drilled in the two bell-shaped ends for

engaging the spokes) which makes the part usable as a bicycle wheel hub.

The third embodiment differs from the second one by the fact that the metallic core is divided in sectors and it is not covered by any deformable sheath. In this embodiment the radial pressure to the tubular body is applied by mechanical means which act on the inside of the core, or by arranging the junctions of the metallic sectors with an elastomeric material, by injecting gas inside the metallic core. After the reticulation of the fabric matrix is obtained, and after a subsequent cooling phase, the internal pressure is stopped and the core comes back to its original dimensions, allowing the two elements of the core to be extracted from the reticulated tubular body.

Finally, the apparatus illustrated in figure 20 can obviously be modified by arranging a wall of high thermal dilatation material of the type shown above in correspondence to the surface of the mould cavity again by using a core made of two metallic material elements 3, 4. In this case, the thermal dilation of the wall of the cavity would determine the application of a radial pressure from the outside inwards on the external surface of the pre-formed tubular body 9 which would thus be squeezed on the metallic core.

Naturally, numerous changes can be implemented to the construction and forms of embodiment of the invention herein envisaged, all comprised within the context of the concept characterising this invention, as defined by the following claims.

For example, despite that this description and accompanying claims explicitly refer to a bicycle wheel hub, the method according to this invention can obviously be applied to manufacturing other components with a similar shape, particularly other bicycle

components. Consequently, also these applications and the deriving products, fall within the scope of this invention.